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AN-8018: FAN9612 400W 4层评估板用户指南 (FEB-279)

飞兆特色产品: FAN9611 / FAN9612

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本用户指南支持可用于交错临界导通模式功率因数校正电源的FAN9612 400W评估板。本用户指南应当与FAN9612数据手册以及飞兆应用指南AN-6086: [“采用FAN9612的交错临界导通模式PFC的设计依据”](#) 配合使用。要了解相关信息, 请访问飞兆半导体网站www.fairchildsemi.com。

1. 评估板概述

FAN9612交错式双临界导通模式(BCM)、功率因数校正(PFC)控制器可控制两个并联的、180°异相的升压系统。交错式功能可将该控制技术的最大实际功率电平从大约300W扩展至800W以上。与常用于更高功率电平的连续导通模式(CCM)技术不同, BCM可以实现升压二极管的零电流开关(不产生反向恢复损耗), 这样就允许在不牺牲效率的情况下采用成本较低的二极管。此外, 输入和输出滤波器的体积更小了, 这是因为传动系统间纹波电流的消除以及开关频率的有效增倍。

带峰值检测的先进前馈线路可在线路瞬变时最大程度减少输出电压变化。为了确保在轻负载条件下稳定运行并具有较少的开关损耗, 最大开关频率箝位至600kHz。在任何工作条件下都能保持同步。

内置保护功能有: 输出过压保护、过流保护、反馈开路保护、欠压闭锁保护、掉电保护和冗余闭锁过压保护。FAN9612采用无铅16引脚SOIC封装。

FAN9612评估板是4层板。针对400W (400V/1A) 额定功率而设计。凭借相位管理功能, 效率在低压线路和高压线路时保持在96%以上, 甚至在额定输出功率低至10%时也是如此。线路电压为115V_{AC}和230V_{AC}时, 满载条件下的效率分别为96.4%和98.2%。

2. 主要特性

- 低总谐波失真、高功率因数
- 180° 异相同步
- 轻负载时的相位自动禁用
- 灌电流为1.8A、拉电流为1.0A的高电流栅极驱动器
- 可减少过冲的跨导(g_m)误差放大器
- 带 $(V_{IN})^2$ 前馈功能的电压模式控制
- 设有可编程软启动时间的闭环软启动, 可减少过冲
- 可避免音频噪声的最低重启频率
- 最大开关频率箝位
- 带软恢复功能的欠压保护
- FB引脚提供非闭锁OVP(过压保护), OVP引脚提供次级闭锁保护
- 开路反馈保护
- 针对每一相位都提供过流和功率限制保护
- 低启动电流: 80 μ A(典型值)
- 兼容 DC 和 50 Hz 至 400 Hz 的 AC 输入进行操作

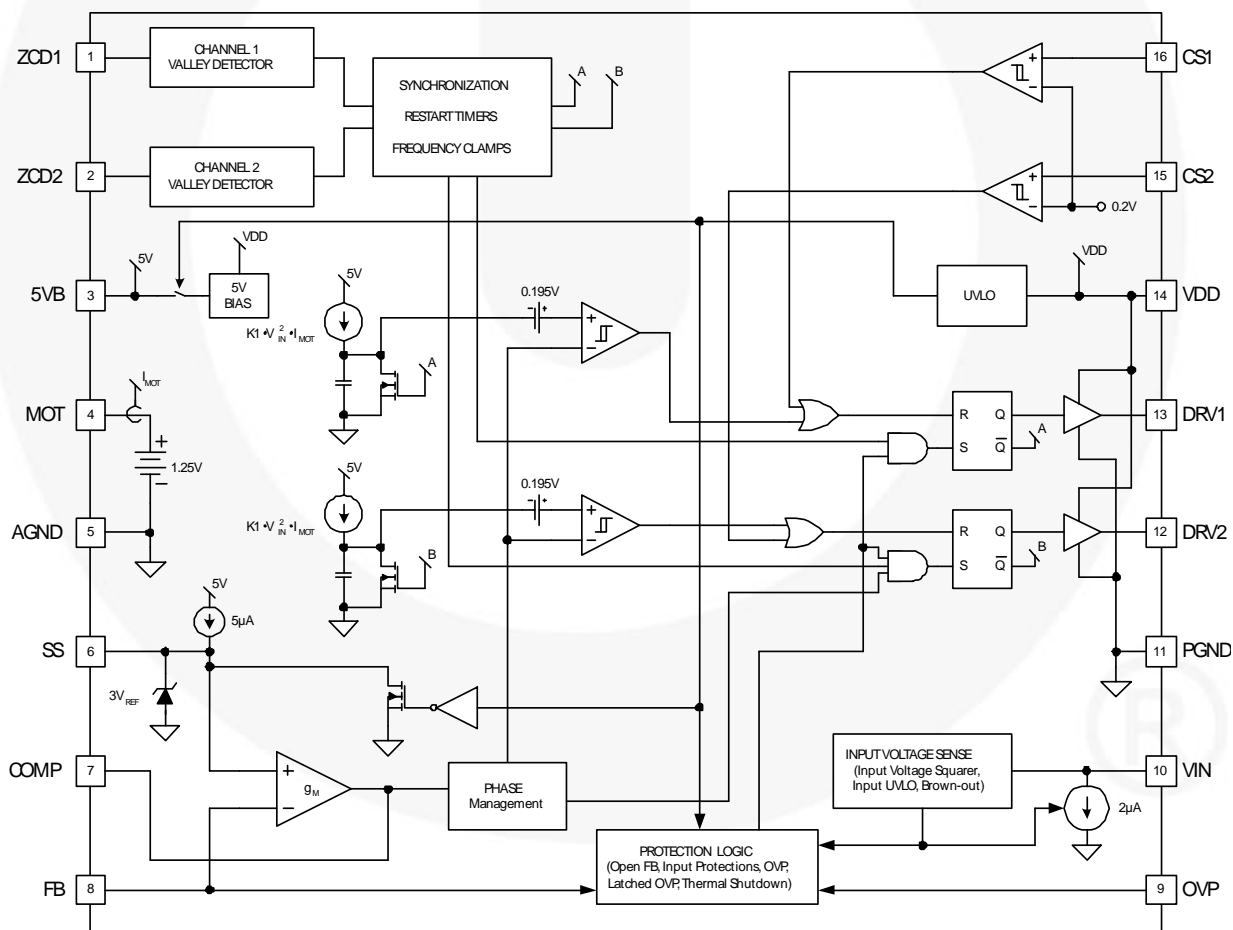


图 1. 框图

3. 规格

该评估板设计和优化时针对的是下列条件：

输入电压范围	额定输出功率	输出电压 (额定电流)
V_{IN} 标称值： 85~265V _{AC} V_{DD} 电源： 13V _{DC} ~18V _{DC}	400W	400V-1A

注意：

1. 20ms保持时间内的最小输出电压为330V_{DC}

- $V_{LINE} = 85\sim 265V_{AC}$
- $V_{OUT} = 400V$
- $f_{SW} > 50kHz$
- 负载低至20%时，效率大于96% (115V_{AC})
- 负载低至20%时，效率大于97% (230V_{AC})
- 满载时PF大于0.98

评估板内置保护功能的跳变点设置如下：

- 非闭锁输出OVP跳变点设定为标称输出电压的108%。
- 闭锁输出OVP跳变点设定为标称输出电压的117%。
- 线路UVLO（掉电保护）跳变点设定为70V_{AC}（10V_{AC}迟滞）。
- 线路OVP跳变点设定为267V_{AC}。
- 每个MOSFET的逐脉冲限流设定为9.1A。

最大功率限值设定为额定输出功率的130%左右。相位管理功能允许在最大功率限值（约150W）的30%处进行切相。输出功率超过最大功率限值（约200W）的40%时，会回到两沟道交错式工作。

4. 测试步骤

测试评估板前； V_{DD} 为直流供电电压，线路输入为交流供电电压，并且作为输出的直流电气负载应当与评估板正确连接。

1. 首先为控制芯片提供 V_{DD} 。该电压应当高于 13V（参见 V_{DD} 导通阈值电压的规格）。
2. 提供 V_{DD} 时，继电器会发出“咔嚓”声。这是正常现象。由于浪涌限流继电器由 5V 参考电压（引脚 3）开启，因此可在 FAN9612 退出 UVLO 时，通过提供高于 13V 的 V_{DD} 开启继电器。

表1. 摘自数据手册的规格

符号	参数	工作条件	最小值	典型值	最大值	单位
电源						
I_{START_UP}	启动电源电流	$V_{DD} = V_{ON} - 0.2V$		80	110	μA
I_{DD}	工作电流	输出未转换		2.5	4.0	mA
I_{DD_DYM}	动态工作电流	$f_{SW} = 50\text{ kHz}; C_{LOAD} = 2nF$		3	5	mA
V_{ON}	UVLO启动阈值电压	V_{DD} 增大	12.0	12.5	13	V
V_{OFF}	UVLO停止阈值电压	V_{DD} 减小	7.0	7.5	8.0	V
	UVLO 滞环			5.0		V

3. 连接交流电压 (85~265V_{AC}) 以启动 FAN9612。由于 FAN9612 具有掉电保护和线路 OVP 功能，因此任何超出工作范围的输入电压都会触发保护。
4. 改变负载电流 (0~1A) 并检查工作状况。评估板设计为输出功率低于 150W 左右时，即进入切相状态。输出功率超过 200W 左右时，即回到两沟道交错式工作。
5. 图 2 中的 Q4 和 D11 允许评估板以低至 8.5V 的低 V_{DD} 电压运行。低 V_{DD} 电压 (8.5~12V) 用作线路电压时，Q4 会首先关断， V_{DD} 通过二极管 D11 充电至 V_{DD} 导通阈值电压，从而允许转换器以低 V_{DD} 电压启动。控制器一启动，Q4 就会开启，D11 就会反向偏置。

5. 原理图

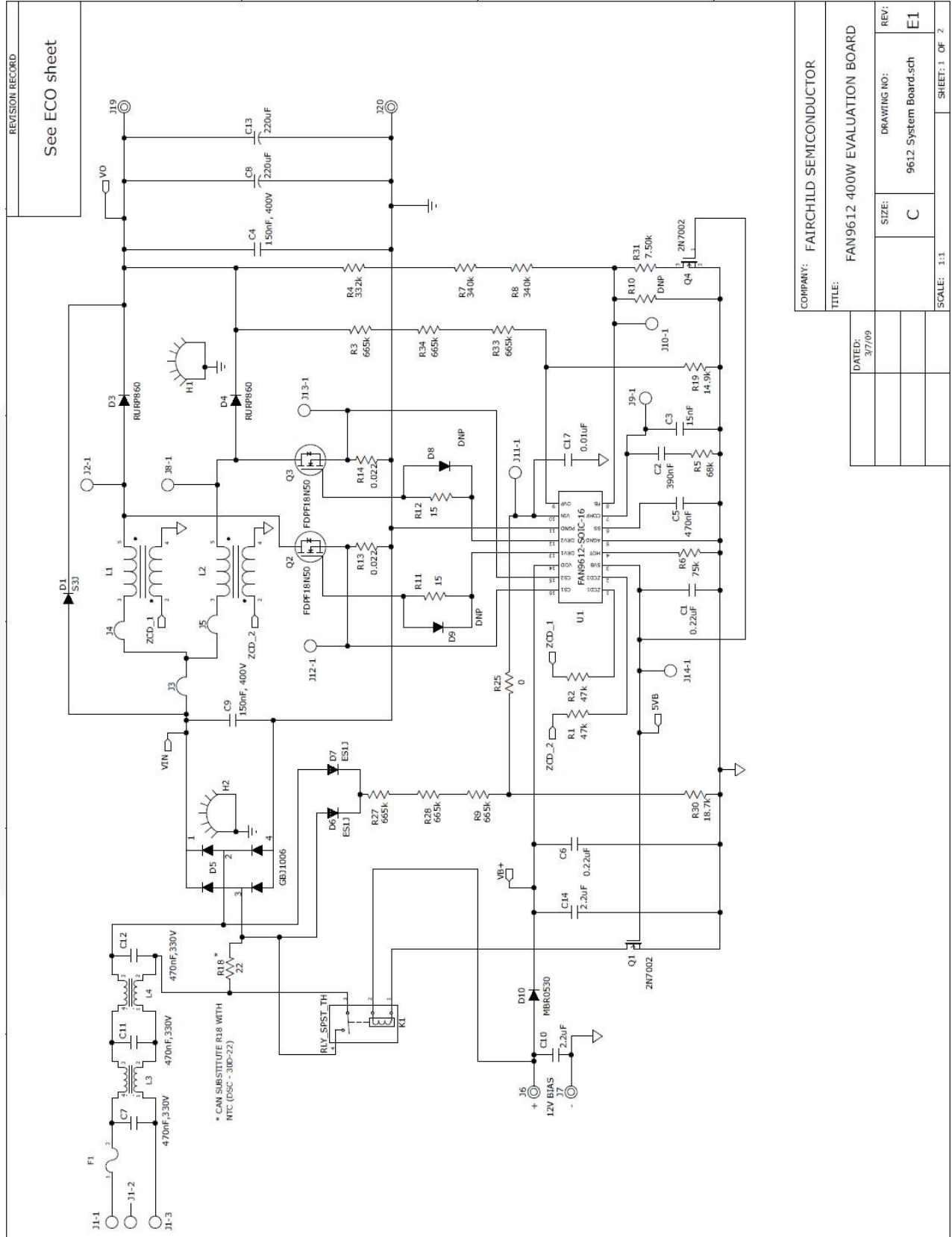


图 2. 400W评估板原理图

6. 升压电感规格

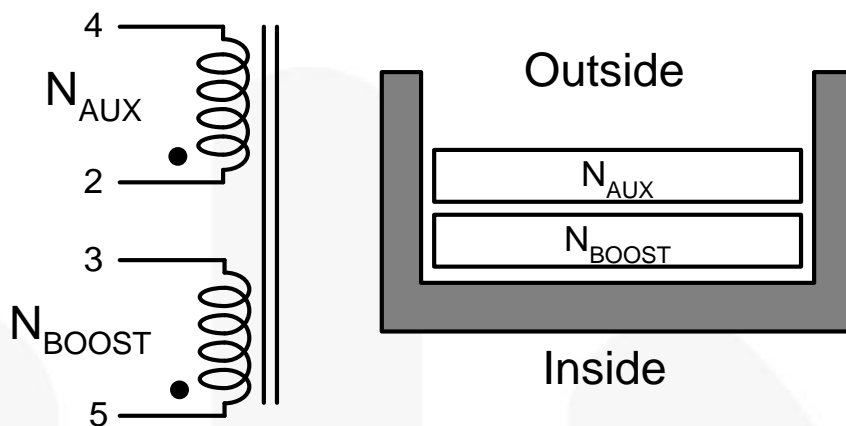


图 3. 评估板使用的升压电感

	引脚	线径/□厚度	匝数
N1	5 → 3	0.1mm × 100 (绞合线)	30
绝缘带		0.05mm	3
N2	2 → 4	0.2mm	3
绝缘带		0.05mm	3

磁芯: PQ3230 ($A_e=161\text{mm}^2$)

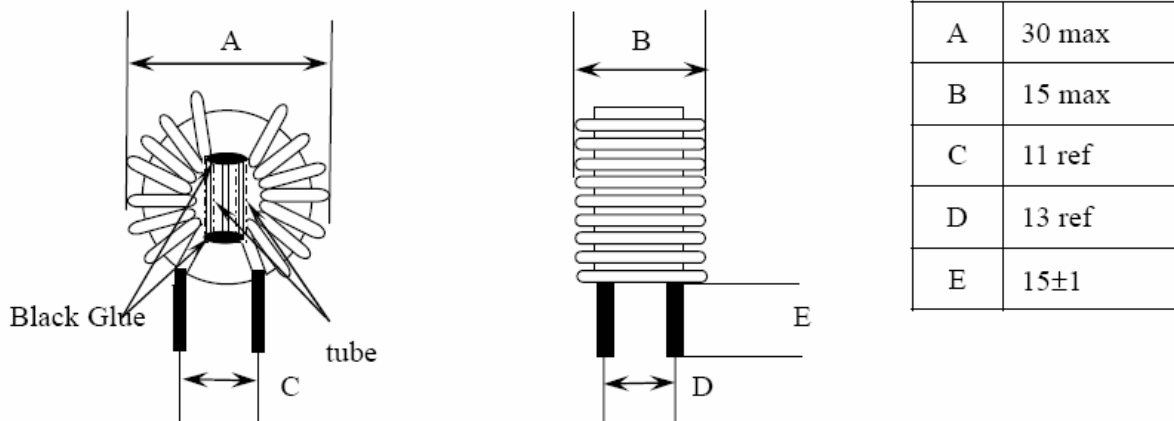
线筒: PQ3230

电感值: 200 μH

7. 线路滤波器电感规格

1. DIMENSION :

UNIT : mm



A	30 max
B	15 max
C	11 ref
D	13 ref
E	15±1

Middle partition board thickness of 2mm
(Safety Regulation)

2. 电气规格: at 1KHz, 1V

- 2.1 电感: $L1=L2 : 9.0\text{mH min}$
- 2.2 直流电阻 $L1=L2: 0.05\Omega$ (最大值)
- 2.3 匝数与导线: $L1=L2: \Phi 0.9 \times 30.5\text{Tsx}2$

图 4. 线路滤波器电感规格

表2. 材料清单

组件	材料	生产厂商	UL文件编号
磁芯	T22x14x08	磁芯T22x14x08, TOMITA	
绕线	THFN-216	Ta Ya Electric Wire Co., Ltd.	E197768
	UEWN/U	PACIFIC Wire and cable Co., Ltd.	E201757
	UEWE	Tai-1 Electric Wire & Cable Co., Ltd.	E85640
	UWY	Jang Shing Wire Co., Ltd.	E174837
焊点	96.5% Sn, 3% Ag, 0.5% Cu	Xin Yuan Co., Ltd.	

8. 材料清单

数量	标号	器件编号	数值	说明	封装类型	生产厂商
2	C1, C6		0.22 μ F	CAP, SMD, CERAMIC, 25V, X7R	805	Vishay
2	C10, C14		2.2 μ F	CAP, SMD, CERAMIC, 25V, X7R	1206	Vishay
1	C17		0.01 μ F	CAP, SMD, CERAMIC, 25V, X7R	805	Vishay
1	C2		390nF	CAP, SMD, CERAMIC, 25V, X7R	805	Vishay
1	C3		15nF	CAP, SMD, CERAMIC, 25V, X7R	805	Vishay
2	C4, C9	ECW-F4154JL	150nF, 400V	电容, 400V, 5%, 聚丙烯	通孔	Panasonic-ECG
1	C5		470nF	CAP, SMD, CERAMIC, 25V, X7R	805	Vishay
3	C7, C11-12	B32914A3474	470nF, 330V	电容, 330V _{AC} , 10%, 聚丙烯	通孔	EPCOS
2	C8, C13	KMH450V220uF	220 μ F	电容, 铝, 电解	通孔	Samyoung
1	D1	S3J		二极管, 600V, 3A, 标准恢复	SMC	飞兆半导体
2	D3-4	RURP860		二极管, 超快速, 600V 8A	T0-220AC	飞兆半导体
1	D5	GBJ1006		桥式整流器, 600V, 10A	通孔	Diodes Inc.
2	D6-7	ES1J		二极管, 快速恢复, 1A 600V	SMA	飞兆半导体
3	D8-9	MBR0530 ⁽³⁾		DIODE SCHOTTKY 30V 500mA SOD123	SOD-123	飞兆半导体
3	D10	MBR0530		二极管, 肖特基, 30V 500mA SOD123	SOD-123	飞兆半导体
1	F1	31.8201		保险丝支架, 5x20mm, 250V _{AC} , 10A	PCB安装, 通孔	Schurter Inc
1	保险丝	0217010.HXP	10A	保险丝, 250V, IEC, FA, LBC, 5x20, 10A, 快速	保险丝盒	Littlefuse Inc.
2	H1-2			散热片		
1	J1	ED100/3DS		端子板, 5MM垂直, 3个位置	通孔	On Shore Technology, Inc.
8	J2, J8-14			通用单引脚连接器(探针)		
3	J3-5			跳线, #16, 绝缘, 用于电流探针测量	通孔	
4	J6-7, J19-20	108-0740-001		连接器, 香蕉插座, 非绝缘, 面板安装	通孔	Emerson Network Power Connectivity Solutions
1	K1	PB134012		RELAY PWR SPST-NO 10A 12VDC PCB	通孔	Tyco
2	L1-2	自定义电感		耦合电感, Pri-30T, Sec-3T, BPQ3230-1112CP	通孔	TDK
2	L3-4	TRN-0197		共模扼流圈	通孔	SEN HUEI INDUSTRIAL CO., LTD
2	Q1, Q4	2N7002		MOSFET, N沟道, 60V 300mA	SOT-123	飞兆半导体
2	Q2-3	FDPF18N50		MOSFET, NCH, 500V, 18A, 0.265 \square	T0-220	飞兆半导体

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BOM (续)

数量	标号	器件编号	数值	说明	封装类型	生产厂商
2	R1-2		47k	RES, SMD, 1/8W	805	Vishay
6	R3, R9, R27-28, R33-34		665k	RES, SMD, 1/8W	805	Vishay
1	R4		332k	RES, SMD, 1/8W	805	Vishay
1	R5		68k	电阻, SMD, 1/8W	805	Vishay
1	R6		75k	RES, SMD, 1/8W	805	Vishay
2	R7-8		340k	RES, SMD, 1/8W	805	Vishay
3	R10		7.5k ⁽³⁾	RES, SMD, 1/8W	805	Vishay
2	R11-12		15	RES, SMD, 1/8W	805	Vishay
2	R13-14		0.022	RES, SMD, 1/2W	1812	Vishay
1	R18		22	电阻本体: 250, 中心: 800	通孔	Vishay
1	R19		14.9k	电阻, SMD, 1/8W	805	Vishay
1	R25		0	电阻, SMD, 1/8W	805	Vishay
1	R30		18.7k	电阻, SMD, 1/8W	805	Vishay
1	R31		7.5k	电阻, SMD, 1/8W	805	Vishay
1	U1	FAN9612		交错式双BCM PFC控制器 1234	S01C-16	飞兆半导体

注意:

3. 不安放。

9. 测试结果

9.1. 启动

图 5和图 6分别显示线路电压为115V_{AC}时，空载和满载条件下的启动运行。由于是闭环软启动，空载启动时仅观察到21V（标称输出电压的5%）的过冲。满载启动时几乎观察不到过冲。

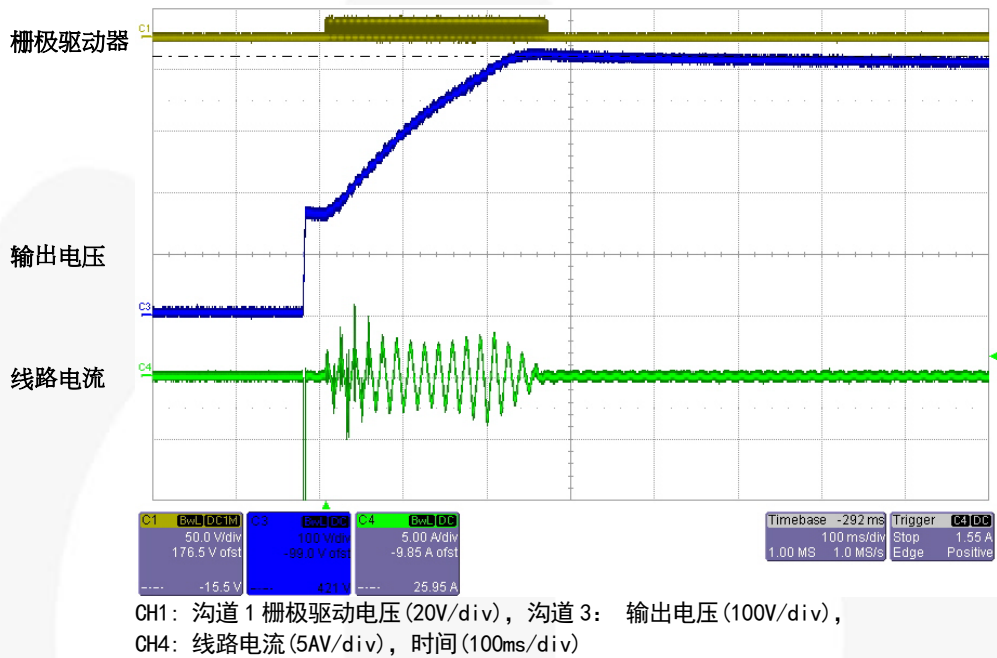


图 5. 115V_{AC}时的空载启动

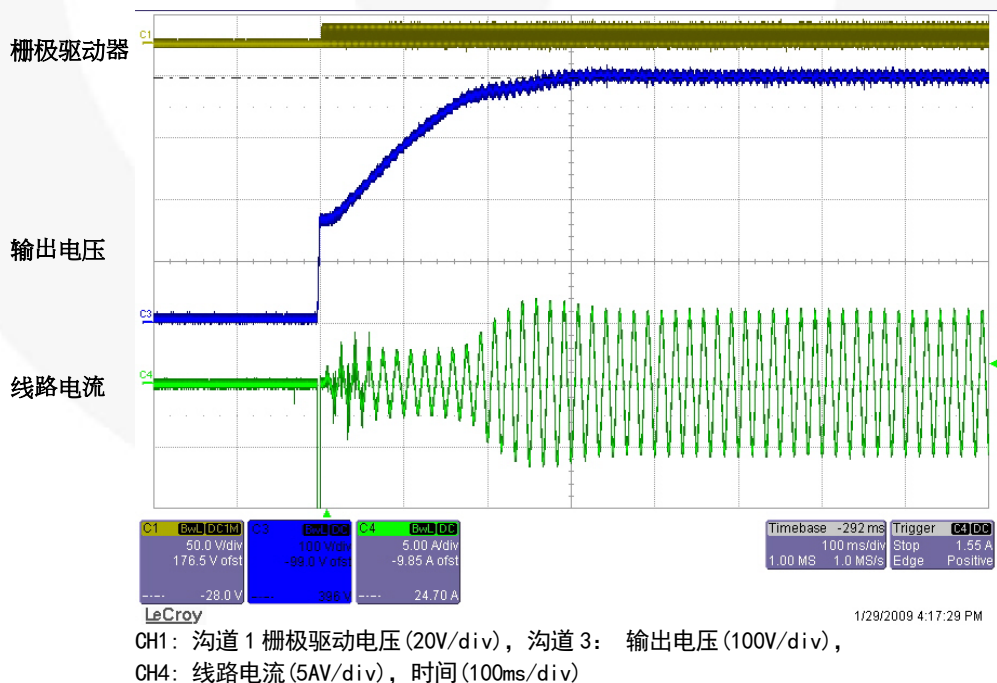
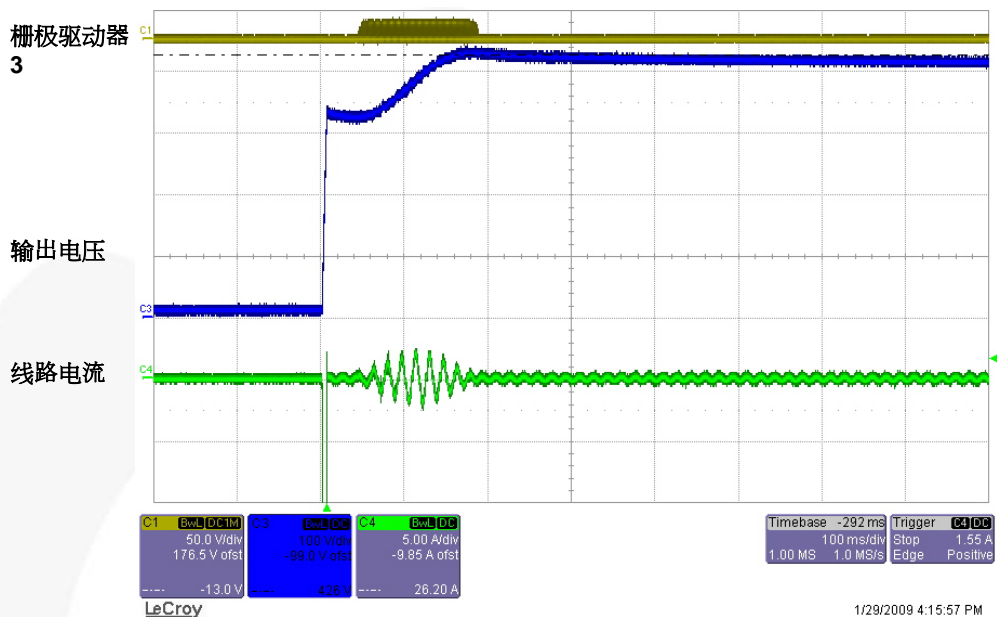


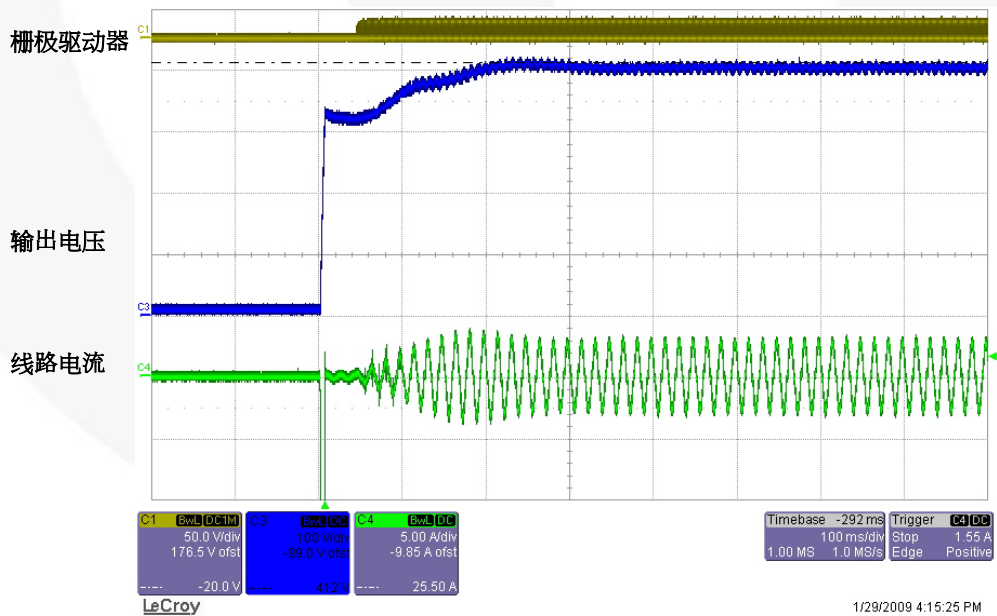
图 6. 115V_{AC}时的满载启动

图 7和图 8分别显示230V_{ac}线路电压时，空载和满载条件下的启动运行。由于是闭环软启动，空载启动时仅观察到26V（标称输出电压的6.5%）的过冲，而满载启动时仅观察到12V（标称输出电压的3%）的过冲。



CH1: 沟道 1 栅极驱动电压 (20V/div), 沟道 3: 输出电压 (100V/div),
CH4: 线路电流 (5A/div), 时间(100ms/div)

图 7. 230V_{ac}时的空载启动

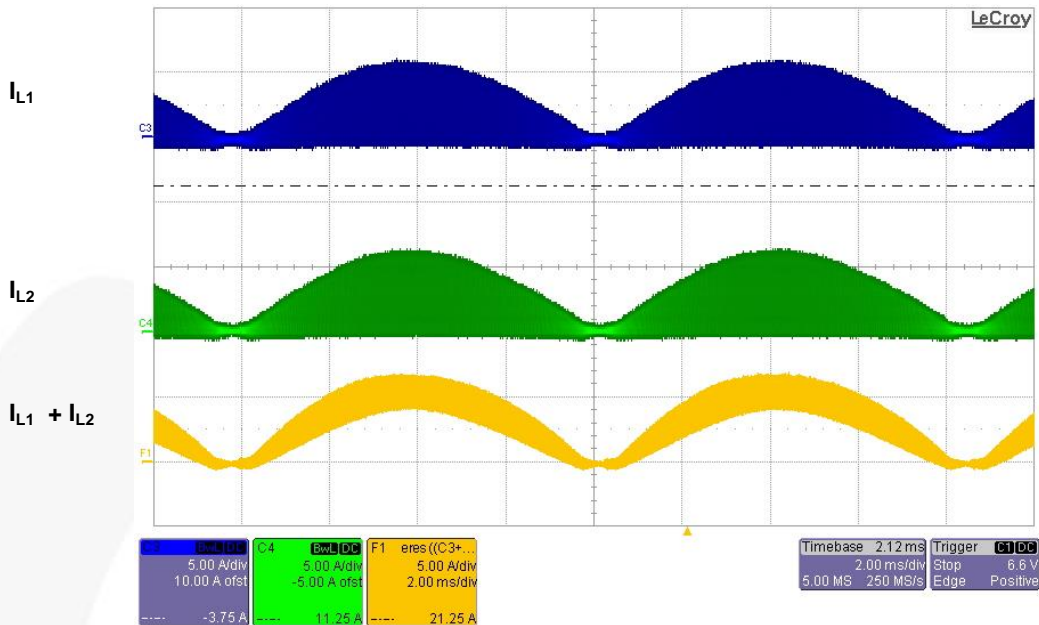


CH1: 沟道 1 栅极驱动电压 (20V/div), 沟道 3: 输出电压 (100V/div),
CH4: 线路电流 (5A/div), 时间(100ms/div)

图 8. 230V_{ac}时的满载启动

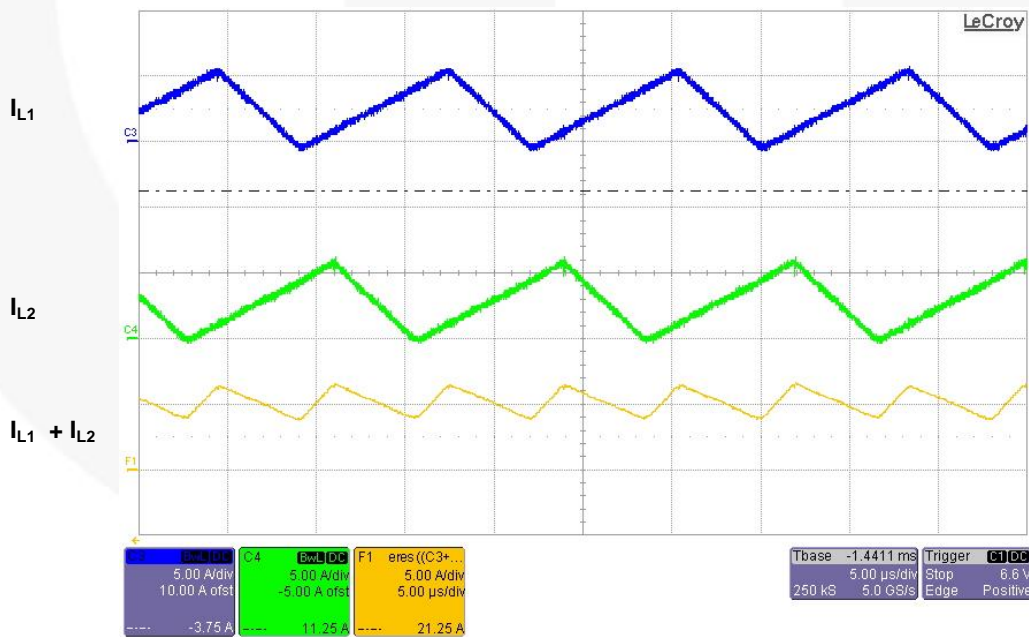
9.2. 正常运行

图 9和图 10分别显示115V_{AC}线路电压以及满载条件下两个电感的电流及两者之和。这两个电感的电流相加后，纹波电流相对较小，这是因为交错工作时纹波相消。



CH3: 电感 L1 电流 (5A/div), 沟道 4: 电感 L2 电流 (5A/div),
F1: 两个电感的电流之和 (5A/div), 时间 (2ms/div)

图 9. 满载和115V_{AC}时的电感电流波形



CH3: 电感 L1 电流 (5A/div), 沟道 4: 电感 L2 电流 (5A/div),
F1: 两个电感的电流之和 (5A/div), 时间 (5μs/div)

图 10. 峰值线路电压时，图 11 中电感电流波形的缩放

图 11和图 12分别显示230V_{AC}线路电压以及满载条件下两个电感的电流及两者之和。这两个电感的电流相加后，纹波电流相对较小，这是因为交错工作时纹波相消。

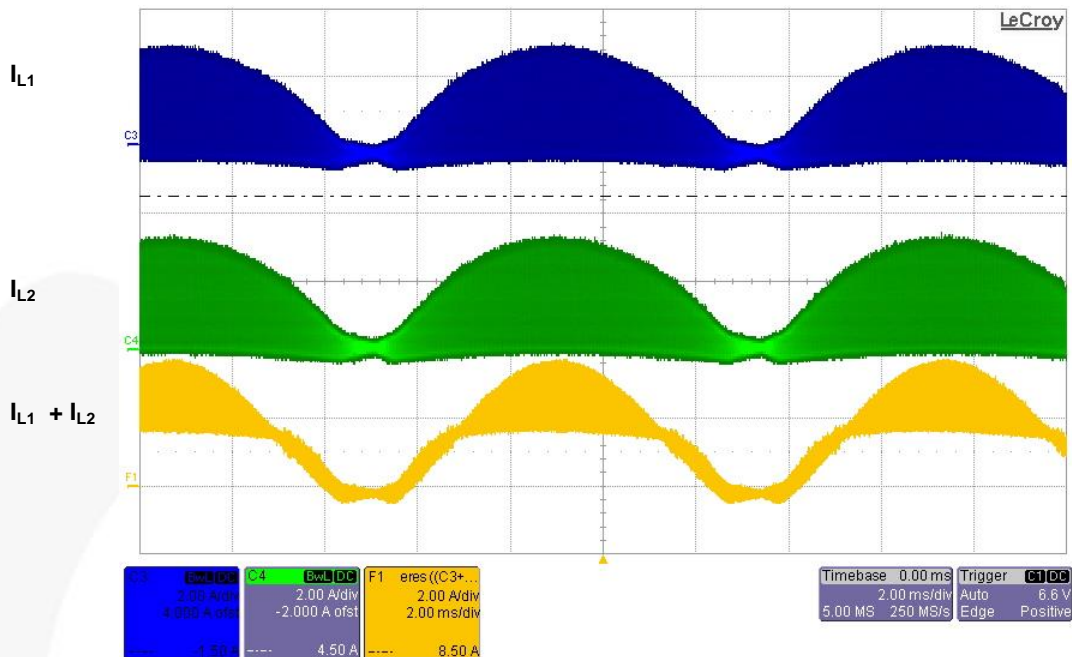


图 11. 满载和230V_{AC}时的电感电流波形

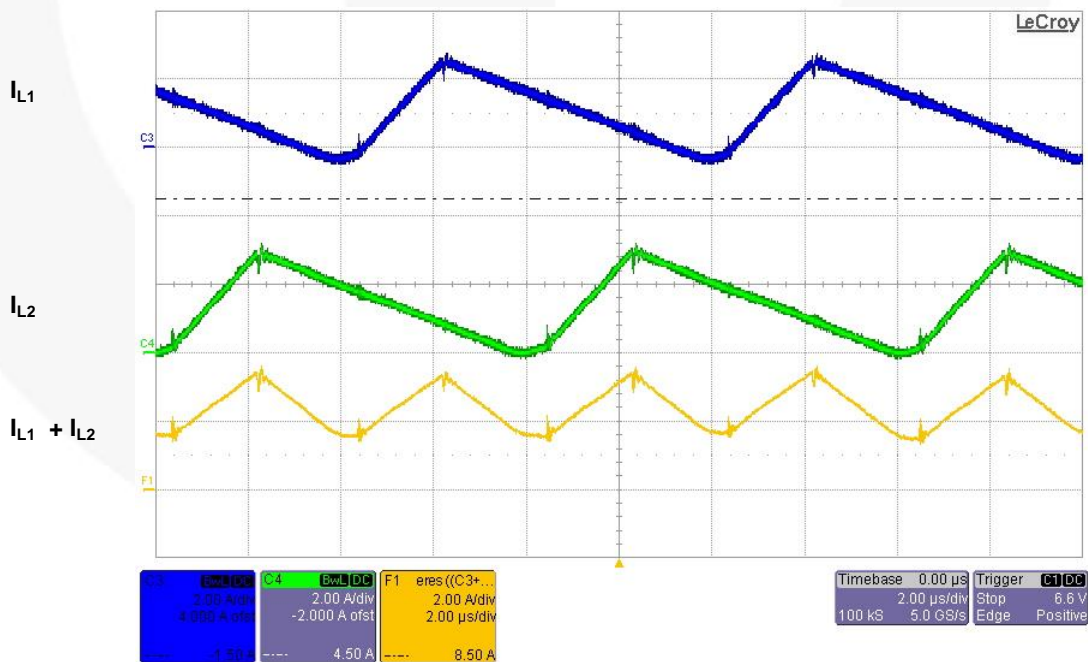
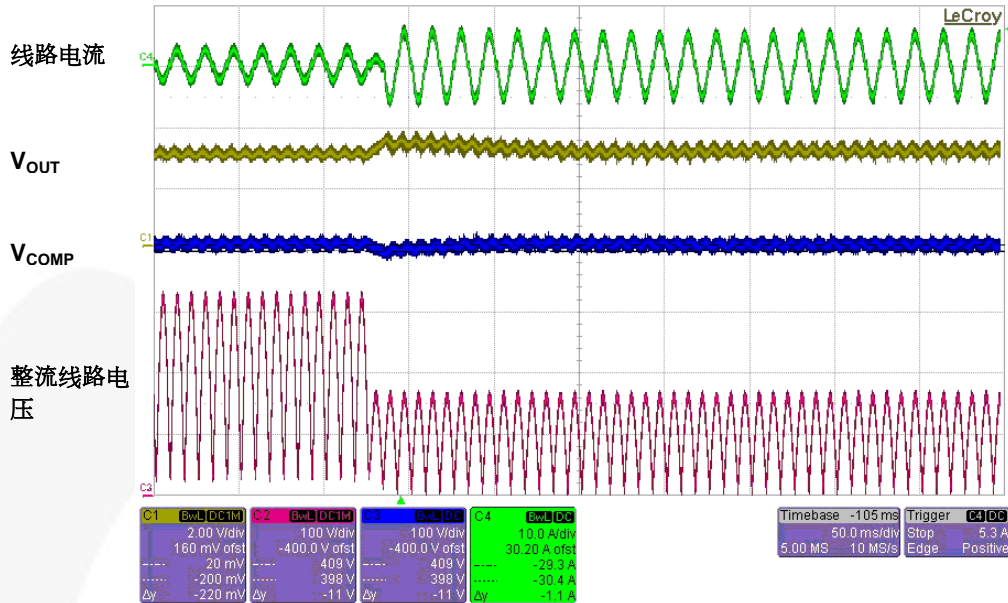


图 12. 峰值线路电压时，图 13中电感电流波形的缩放

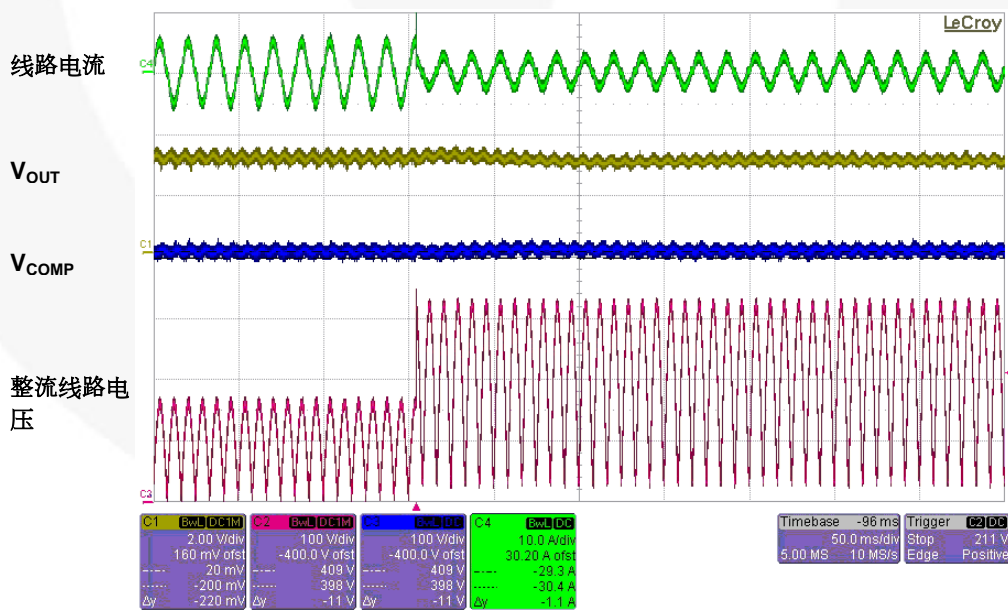
9.3. 线路瞬变

图 13和图 14显示的是线路瞬变操作以及线路前馈功能对输出电压的最小效应。线路电压从230V_{AC}变为115V_{AC}时，可观察到11V（标称输出电压的2.8%）的欠冲。线路电压从115V_{AC}变为230V_{AC}时，几乎观察不到有电压欠冲。



CH1: COMP 引脚电压 (2V/div), 沟道 2: 整流线路电压 (100V/div)
CH3: 输出电压 (100V/div), 沟道 4: 线路电流 (10A/div), 时间 (50ms/div)

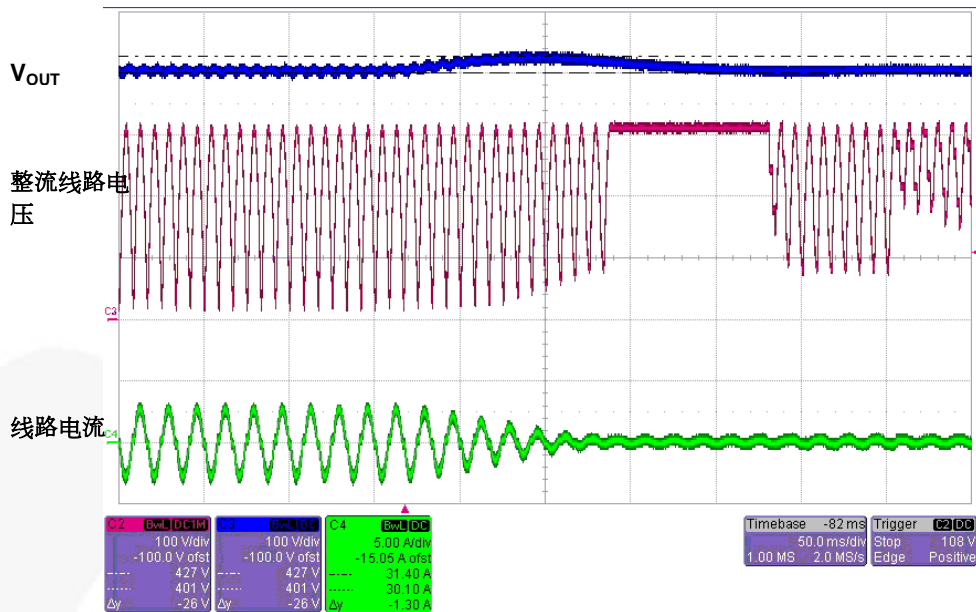
图 13. 满载条件下的线路瞬变响应 (230V_{AC} → 115V_{AC})



CH1: COMP 引脚电压 (2V/div), 沟道 2: 整流线路电压 (100V/div)
CH3: 输出电压 (100V/div), 沟道 4: 线路电流 (10A/div), 时间 (50ms/div)

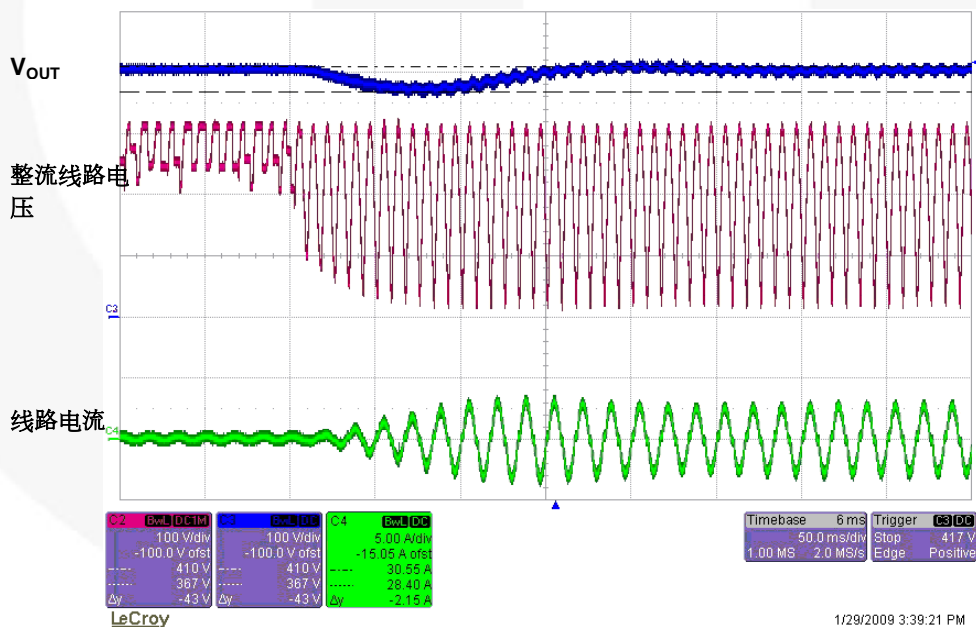
图 14. 满载条件下的线路瞬变响应 (115V_{AC} → 230V_{AC})

图 15和图 16显示的是负载瞬变操作。输出负载从100%变为0%时，可观察到26V（标称输出电压的6.5%）的过冲。输出负载从0%变为100%时，可观察到43V（标称输出电压的11%）的欠冲。



CH2: 整流线路电压(100V/div), 沟道3: 输出电压(100V/div),
沟道4: 线路电流(10AV/div), 时间(50ms/div)

图 15. 230V_{ac} (满载→空载) 时的负载瞬变响应

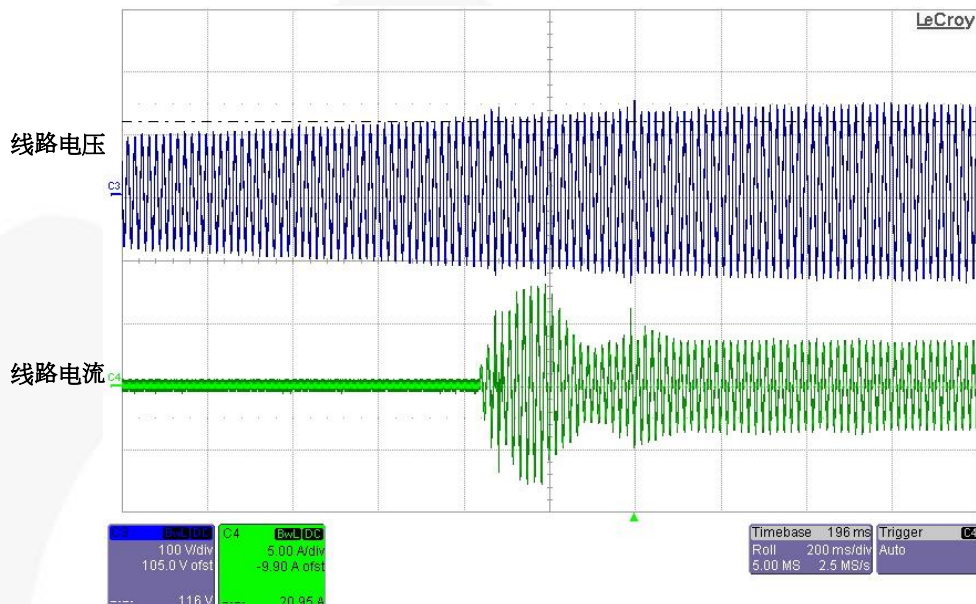


CH2: 整流线路电压(100V/div), 沟道3: 输出电压(100V/div),
沟道4: 线路电流(10AV/div), 时间(50ms/div)

图 16. 230V_{ac} (空载→满载) 时的负载瞬变响应

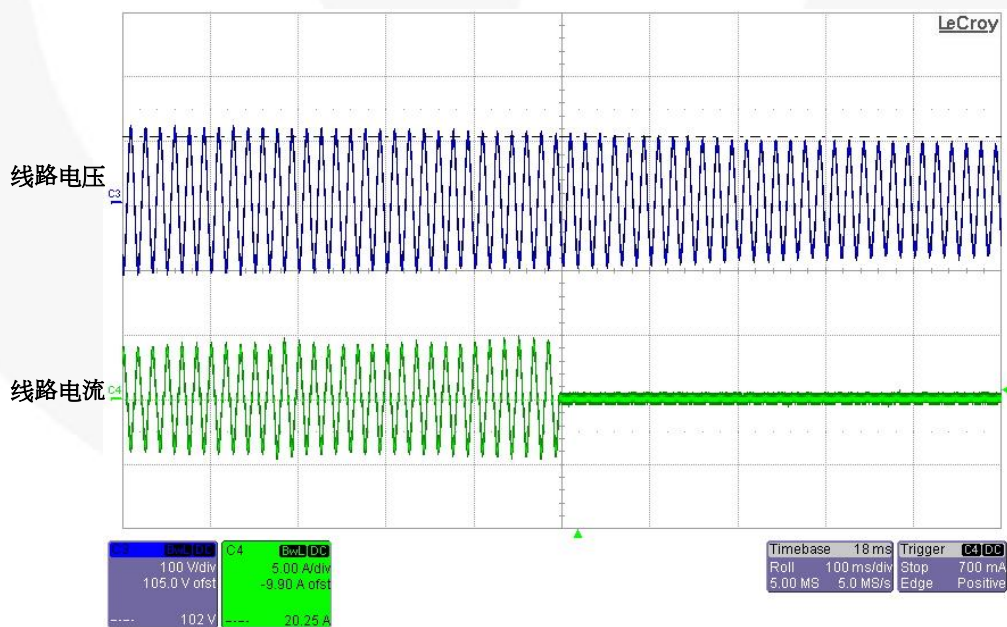
9.4. 掉电保护

图 17和图 18分别显示的是线路电压缓慢上升和缓慢下降时的启动与关断操作。线路电压达到大约80V_{AC}时，电源开启；线路电压下降至70V_{AC}以下时，电源关断。



CH3: 线路电压(100V/div), 沟道 4: 线路电流(5A/div), 时间(100ms/div)

图 17. 缓慢增大线路电压的情况下开启

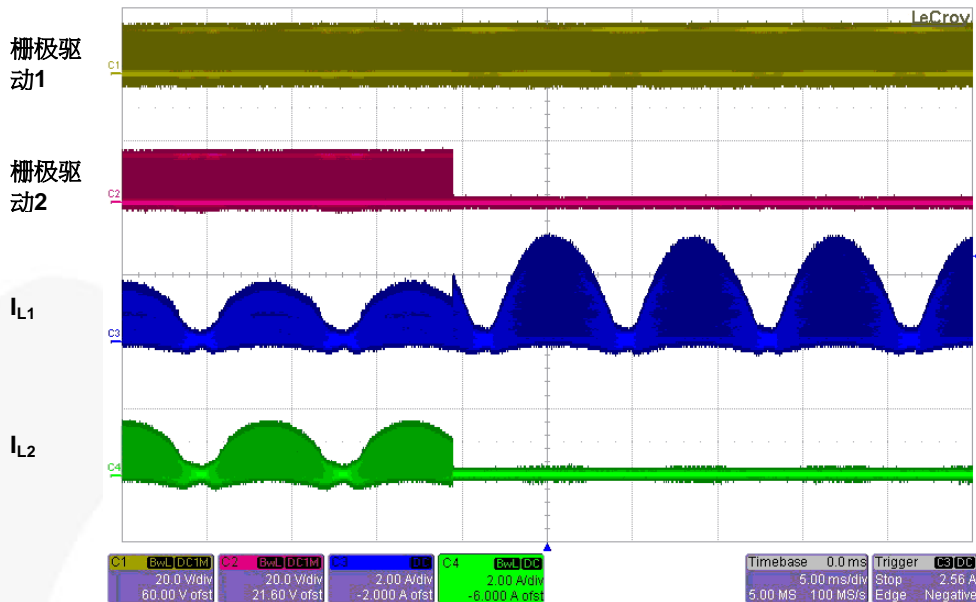


CH3: 线路电压(100V/div), 沟道 4: 线路电流(5A/div), 时间(200ms/div)

图 18. 缓慢减小线路电压的情况下关断

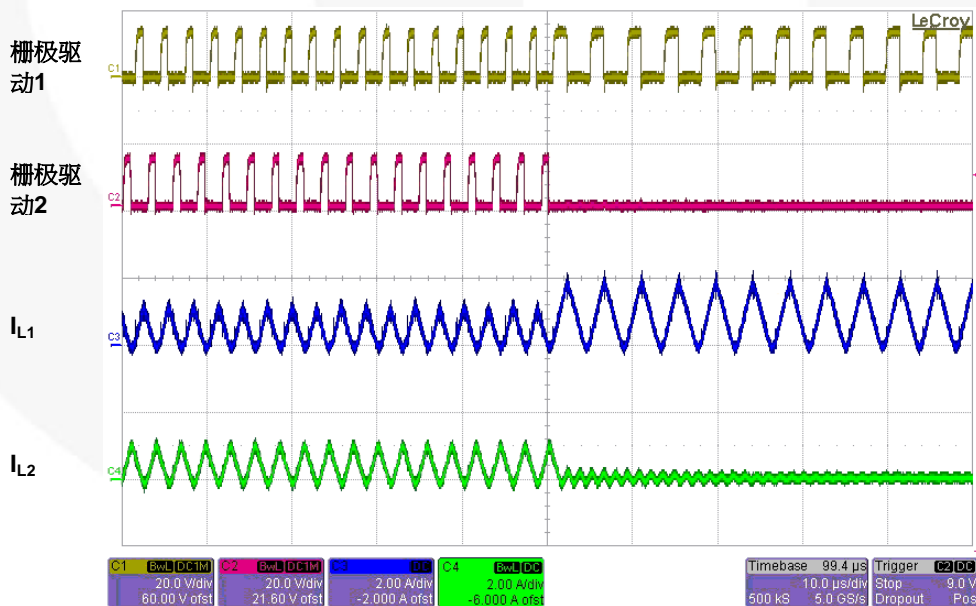
9.5. 相位管理

图 19和图 20显示的是切相波形。如图所示，沟道1栅极驱动信号的占空比在其他通道栅极驱动信号禁用时倍增，实现最少的线路电流干扰。



CH1: 沟道 1 栅极驱动电压 (20V/div), 沟道 2: 沟道 2 栅极驱动电压 (20V/div), 沟道 3: 电感 L1 电流 (5A/div), 沟道 4: 电感 L2 电流 (5A/div), 时间 (5ms/div)

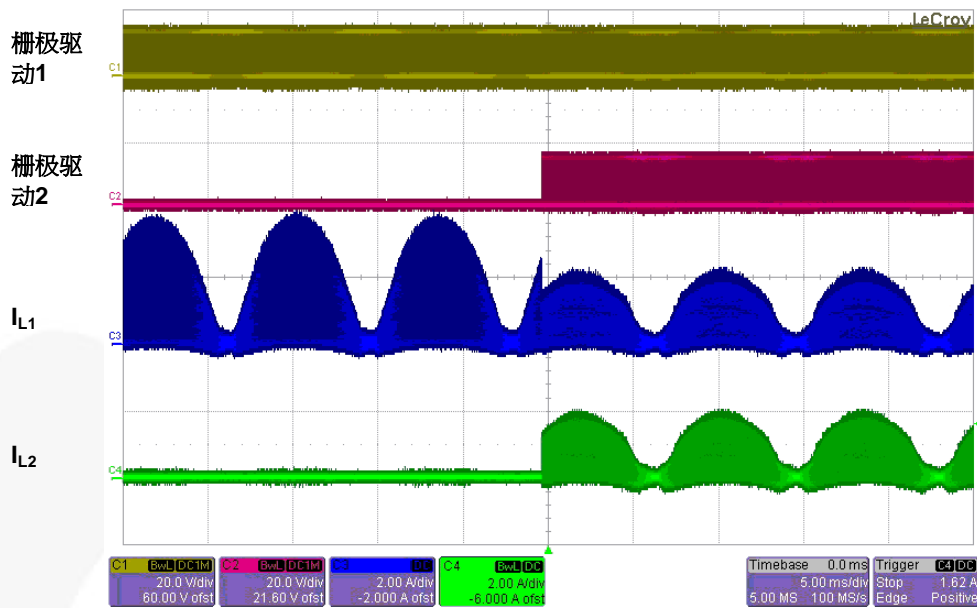
图 19. 切相操作



CH1: 沟道 1 栅极驱动电压 (20V/div), 沟道 2: 沟道 2 栅极驱动电压 (20V/div), 沟道 3: 电感 L1 电流 (5A/div), 沟道 4: 电感 L2 电流 (5A/div), 时间 (10μs/div)

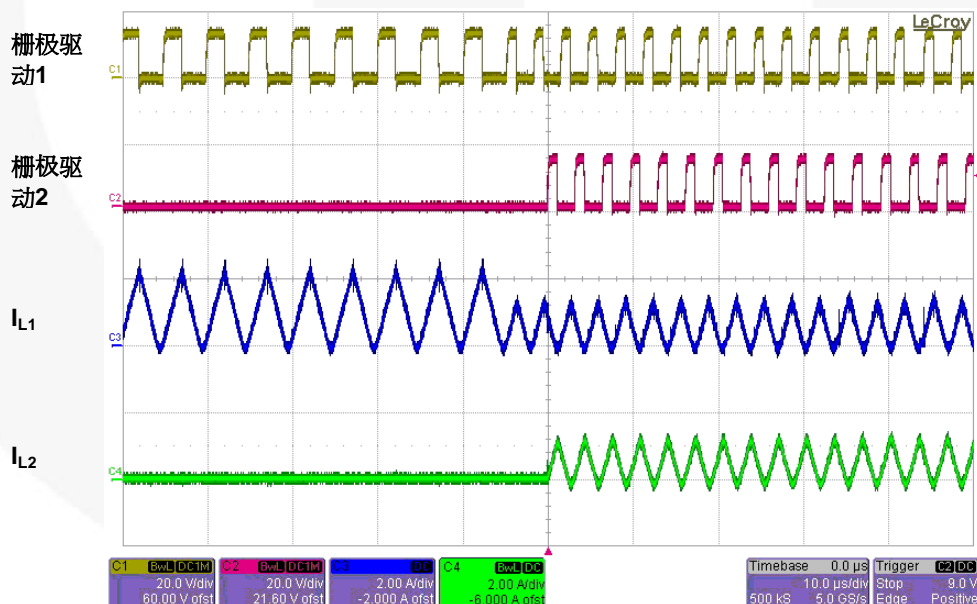
图 20. 切相操作

图 21和图 22显示的是相位叠加波形。如图所示，沟道1栅极驱动信号的占空比在其他通道栅极驱动信号使能时减半，实现最少的线路电流干扰。



CH1: 沟道 1 栅极驱动电压 (20V/div), 沟道 2: 沟道 2 栅极驱动电压 (20V/div), 沟道 3: 电感 L1 电流 (5AV/div), 沟道 4: 电感 L2 电流 (5AV/div), 时间 (5ms/div)

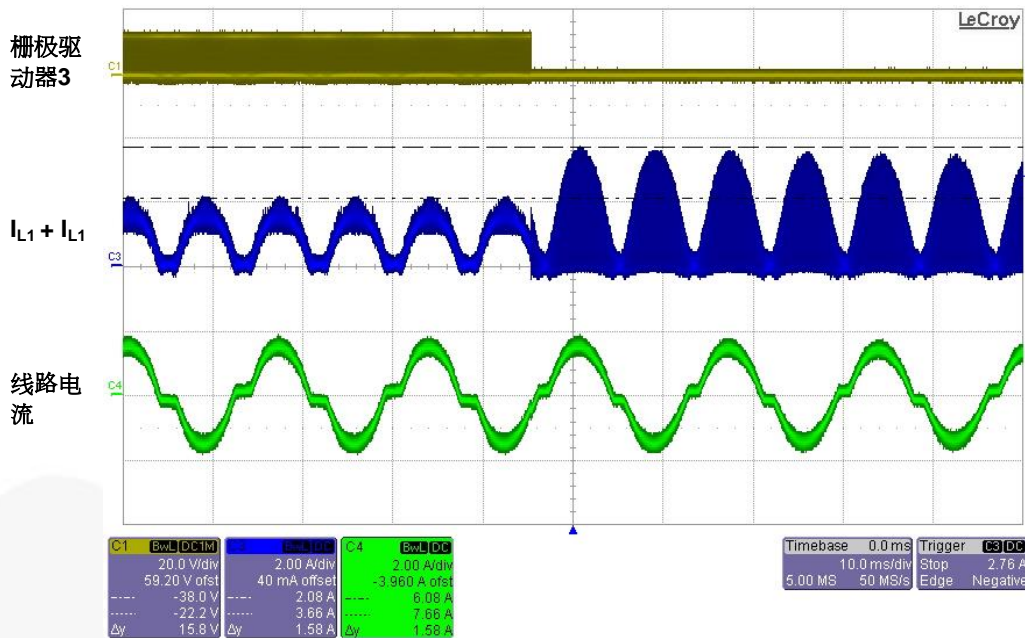
图 21. 相位叠加操作 (放大)



CH1: 沟道 1 栅极驱动电压 (20V/div), 沟道 2: 沟道 2 栅极驱动电压 (20V/div), 沟道 3: 电感 L1 电流 (5AV/div), 沟道 4: 电感 L2 电流 (5AV/div), 时间 (10μs/div)

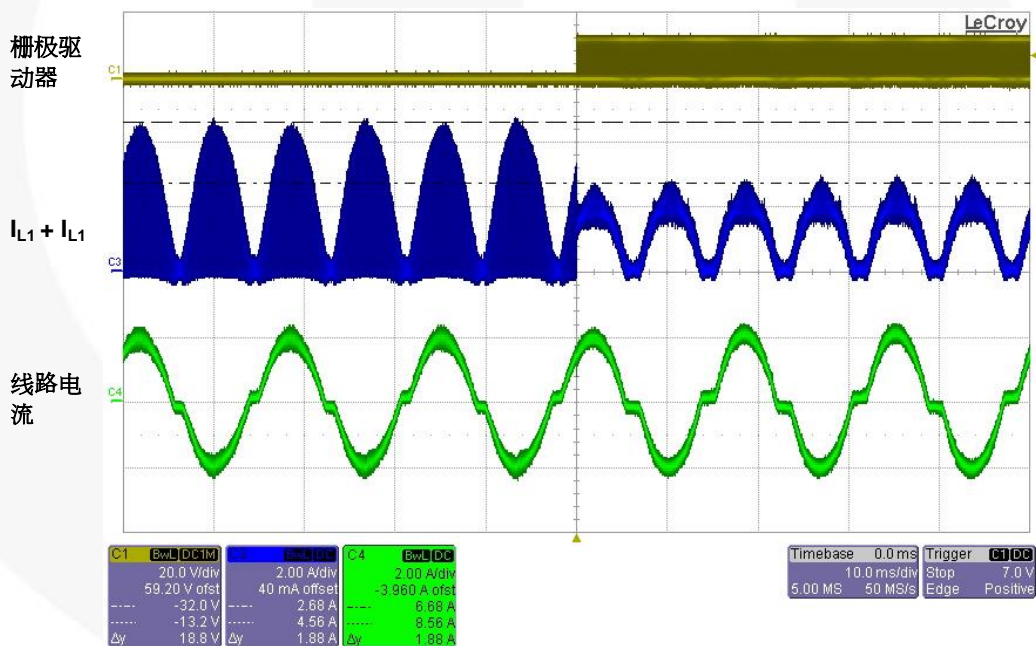
图 22. 相位叠加操作 (放大)

图 23和图 24分别显示的是两个电感的电流之和以及切相和相位叠加时的线路电流。如图所示，相位管理功能未明显改变线路电流波形。



CH1: 沟道 2 栅极驱动电压 (20V/div), 沟道 3: 两个电感的电流之和 (2A/div),
沟道 4: 线路电流 (2A/div), 时间 (10ms/div)

图 23. 切相和线路电流



CH1: 沟道 2 栅极驱动电压 (20V/div), 沟道 3: 两个电感的电流之和 (2A/div),
沟道 4: 线路电流 (2A/div), 时间 (10ms/div)

图 24. 相位叠加操作和线路电流

9.6. 效率

图 25和图 26显示的是输入电压分别为115V_{AC}和230V_{AC}时测得的评估板（有/无相位管理功能）的效率。这些曲线表明相位管理功能在轻载条件下可提升1%至7%的效率，具体取决于线路电压和负载条件。由于切相通过有效降低轻载时的开关频率可减少开关损耗，因此在开关损耗较高的高压线路上，效率能提高更多。低压线路上的效率相对提高较少，这是因为MOSFET以零电压开启，开关损耗忽略不计。

由于外部电源用于V_{DD}，因此控制IC的功耗未包含在内，但其数值非常小(<1W)。

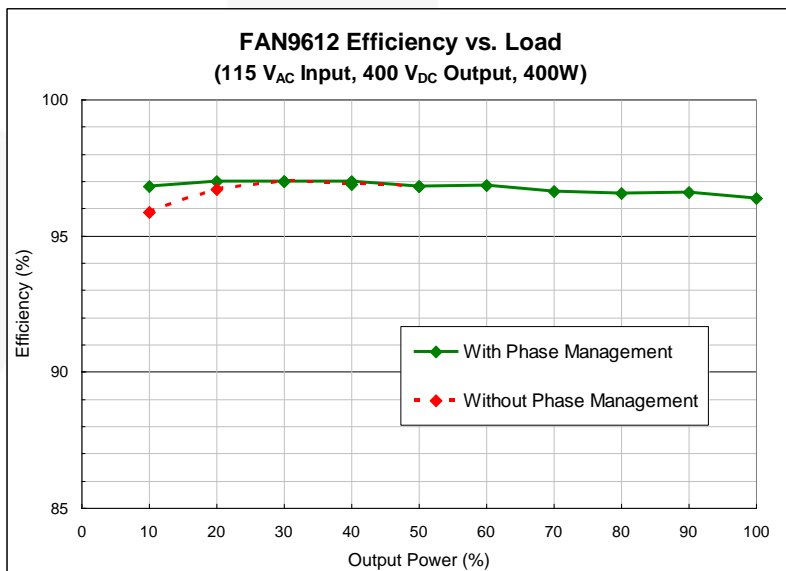


图 25. 115V_{AC}时测得的效率

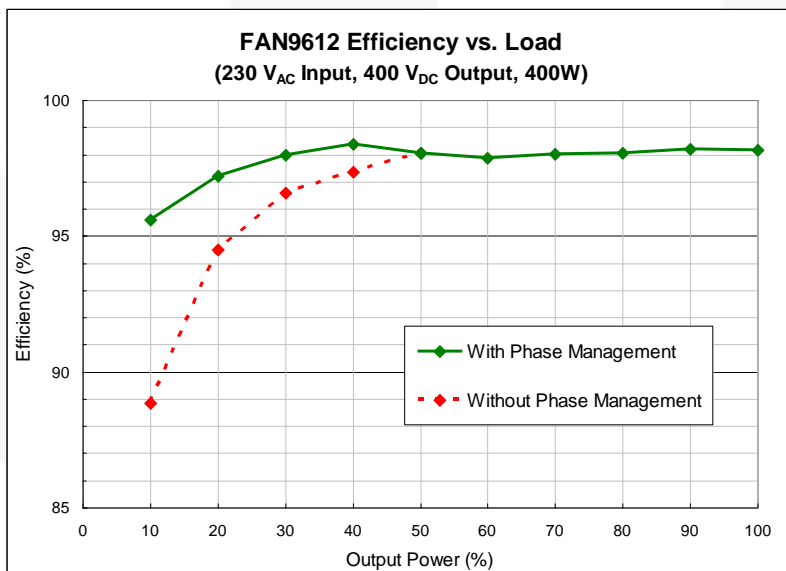


图 26. 230V_{AC}时测得的效率

9.7. 谐波失真和功率因数

图 27和图 28分别采用EN61000 D类和C类规范比较输入电压为115V_{AC}和230V_{AC}时测得的谐波电流。D类规范适用于电视机和PC电源，C类规范适用于照明应用。从图中可以看出，两种规范均得到了满足，且裕量足够。

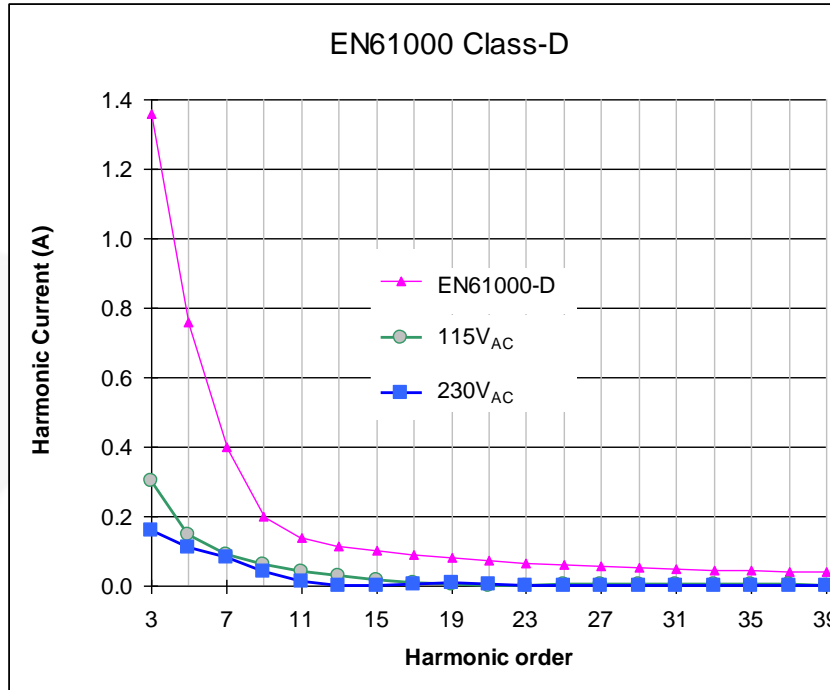


图 27. 测得的谐波电流和EN61000 D类规范

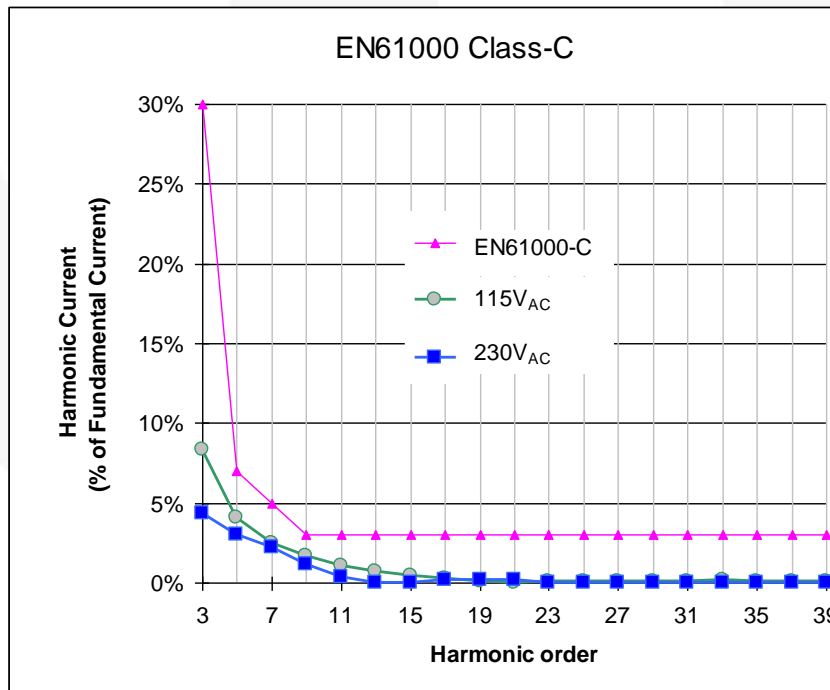


图 28. 测得的谐波电流和EN61000 C类规范

图 29显示的是输入电压为115V_{AC}和230V_{AC}时测得的功率因数。从图中可以看出，高于0.98的高功率因数可在100%至50%负载处得到。表3显示的是输入电压为115V_{AC}和230V_{AC}时的总谐波失真。

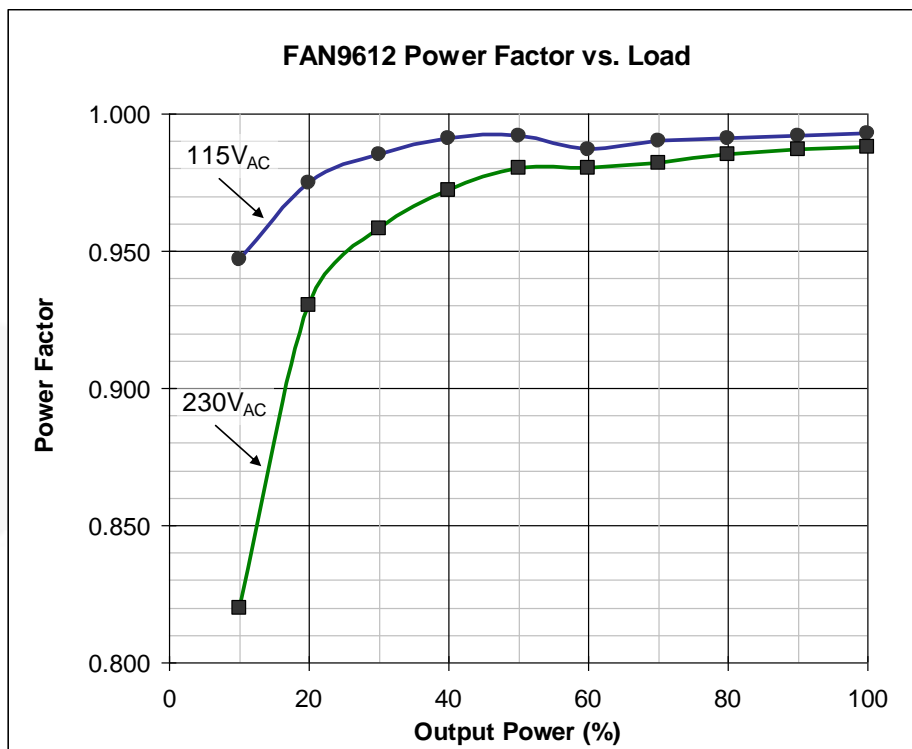


图 29. 测得的功率因数

表3. 总谐波失真(THD)

线路电压	100%负载	75%负载	50%负载
115V _{AC}	9.9%	12.3%	16.35%
230V _{AC}	11.98%	13.82%	16.29%

10. 参考文献

[FAN9611 / FAN9612 — 交错式双 BCM PFC 控制器](#)

[AN-6086 — 采用FAN9612的交错临界导通模式 \(BCM\) PFC的设计依据](#)

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FEB279	FAN9611 / FAN9612 400W评估板

12. 修订记录

日期	修订版 #	说明
2009年2月20日	0.0.1	初始版
2009年4月7日	0.0.2	原理图和BOM更新
2009年4月9日	0.0.3	更正
2010 年 3 月	0.0.4	更正了屏幕截图 警告与声明更新
2010 年 5 月	0.0.5	为清晰起见, 更改了标题
2010 年 6 月	0.0.6	更新到包含FAN9611

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